

A Study About Some Mechanical Properties for Composites Reinforced with Corn Cob Powder

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Abstract: In this paper we have created some composites reinforced with corn cob powder and the matrix was made by a combination between Resoltech 1050 resin with its Resoltech 1058 hardener. For the composites manufacturing, we have used the manual casting technique. For the new manufactured composites, we have determined the mechanical properties from the tensile test according to ASTM D3039: Young modulus, breaking strength and elongation at break. We have also molded samples for the compression test according to ASTM D695-15 and we have determined the breaking strength. The tensile and compression tests were made on universal testing machines. In the end, we have determined also the dynamic mechanical properties for the studied material by clamping the samples at one edge and leaving the samples unconstrained at the other edge. At the unconstrained edge we have placed a Bruel&Kjaer accelerometer which recorded the samples free vibrations. From the free vibrations recording and Euler-Bernoulli theory, we have determined the next dynamic mechanical properties: damping factor per unit mass and length, eigenfrequency, dynamic modulus of elasticity, loss factor and dynamic rigidity. From the experimental results, we have obtained increased breaking strength values for the proposed material at compression compared to the tensile test. Compared to similar materials studied in the engineering literature, we have obtained increased compression breaking strength.

Keywords: epoxy resin, corn cob, powder, vibrations, tensile, compression

1. Introduction

The corn cob is a solution to reinforce composite materials [1-4]. In [4] there were used samples with corn cob powder, E-glass and epoxy resin. From the tensile test, there were obtained values between 14..18 MPa for the breaking stress and 650..900 for the modulus of elasticity. From the bending test, values between 27 and 37 MPa for the breaking stress and between 3200 up to 4600 for the modulus of elasticity were obtained. Lignosulfonates or sulfonated lignin are water-soluble polyelectrolytic polymers which are obtained from lignin, a polymer from phenylopropane units. They are by-products of the wood pulp production using sulphite pulp [5]. The sulphite pulp refers to wood chips that are treated with sulphite and bisulphite ions solutions. In [6], some composites with lignosulphonate matrix and corn cob powder were built. There were used particles sizes between 0.090 and 1.8 mm and reinforcement proportion between 10 and 35%. There were obtained maximum values for the compression breaking strength of 20 MPa and 320 MPa for the Young modulus.

There were made researches for integrating the corn stalk in civil constructions. In this way, in [7], there are presented researches regarding inserting the corn stalks in building isolation combined with cement from magnesium phosphate. The mixture between those parts fulfill the conditions for being used in civil contructions.

In [8], some green composite materials were made using the thermoplastic matrix of corn starch and fibers from corn husk. Those corn husk fibers were used as a filler. The materials were manufactured by a molding method using different proportions of husk fiber (between 0-8%) and fructose as a plasticizer at a fixed amount of ¼ for the corn starch weight. The physical, thermal, morphological and tensile

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Mater. Plast., 58 (4), 2021, 1-8

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characteristics of composites were investigated. Values between 6 and 13 MPa for the breaking stress, 90 and 650 MPa for the modulus of elasticity and 2.5 and 7% elongation at break values.

The research from [9] deals with the investigation for corn starch by using a X-ray diffraction technique and thermal analysis. There was also investigated the manufacturing and characterization for starch fiber composites - banana and sugar cane. The thermal analysis has shown a good thermal stability for the composites manufacturing. There were also determined some mechanical characteristics from the tensile test: Young modulus between 24.6 and 468.2 MPa, breaking stress between 1.7 and 4MPa, elongation at break between 2.7 and 75.5%.

In this paper we have manufactured some composite materials from corn cob powder as a reinforcement and the epoxy resin as a matrix. The corn was brought in a powder shape by using a classic mill.

2. Materials and methods

In this research we have obtained some composite materials by using the con cob powder as reinforcement and the epoxy resin RESOLTECH 1050 with the hardener RESOLTECH 1058. The resin mechanical properties can be found in [10].

2.1. Tensile test

For the tensile test, we have manufactured, by manual casting, a plate with the dimensions of 420x297 mm. The plate had a thickness of 8 mm. We have used a proportion of 65% corn stalk powder and 35% epoxy resin. From this plate we cut ten samples for the tensile test. Some of the samples used in this test are presented in Figure 2, with the dimensions 200 x 25 x 8 mm. We have used the standard ASTM D3039 for the tensile test [11].



E-0-4 P-0-14 P-0-14

Figure 1. The plate obtained from the manual casting

Figure 2. Some samples used for the tensile test

2.2. Compression test

We have chosen to test the proposed material to compression because we have assumed that the studied material could have a behaviour similar to the concrete: a low tensile strength compared to the compression one. For this test, we have used the next proportions: 50%, 65% and 75% corn cob powder and 50%, 35% and 25% epoxy resin respectively. We have used the standard ASTM D695-15 for the compression test [12]. The samples dimensions were $\Phi 30x60$ mm with cylindrical shape and there were casted ten samples from each proportion reinforcement - matrix cathegory. An example with the samples used for the compression test having 50% epoxy resin and 50% corn cob powder is presented in Figure 3.





Figure 3. Some samples used for the compression test, with 50% corn cob powder

2.3. Vibrations tests

We have determined some mechanical parameters through the vibrations test, such as: the damping factor reported to the unit mass and length, the eigenfrequency, the dynamic modulus of elasticity, the dynamic rigidity and the loss factor for some with 65-35 reinforcement-matrix ratio. The bars were embedded at one end with a jaw vise on a rigid table, each bars having 100, 120, 140, 160 and 180 mm free lengths. We have tested ten samples for each free length. On the free end, at about 5 mm from the edge, on the longitudinal axis, the Bruel&Kjaer accelerometer was glued by wax on the sample. For each assembly condition of the bars type and free length, an initial displacement was applied to the bar and then, by releasing, the bar performed free damped vibrations. To study the vibrations, the next equipment was used: an accelerometer Bruel&Kjaer that had the sensitivity 4/1000 pC/ms⁻² connected to a signal amplifier NEXUS 2692-A-0I4 which was connected with a data acquisition system SPIDER 8. The SPIDER 8 apparatus was connected by USB with a laptop. The link between the two entities is made through CATMAN EASY software.

From the free vibrations experimental recording in a certain point, we can determine the damping factors related to unit mass and length by using the relationships (1) and (2) [13].

$$\mu = \frac{1}{t_2 - t_1} \ln \frac{v_1}{v_2} \tag{1}$$

$$C = \frac{2}{t_2 - t_1} \ln \frac{v_1}{v_2} \langle \rho A \rangle \tag{2}$$

In (1) and (2) we have marked with t_1 and t_2 the time values for two peaks in the free vibrations diagram; v_1 is the amplitude maximum value that corresponds to t_1 time and v_2 is the amplitude maximum value that corresponds to t_2 time; $\langle \rho A \rangle$ is the specific mass.

The other experimental values are determined with (3), (4) and (5) according to [13].

$$\eta = \frac{\mu}{\pi \cdot \nu} \tag{3}$$

$$E = \frac{12 \cdot \rho \cdot l^4 \cdot v^2}{\lambda^2 \cdot t^2} \tag{4}$$



$$EI = \frac{4 \cdot \pi^2 \cdot \rho \cdot A \cdot l^4 \cdot v^2}{\zeta^2} \tag{5}$$

In (3), (4) and (5) are presented the next mechanical parameters: v the eigenfrequency, l the sample free length, λ a constant from the samples fixing condition (0.5596 for our case, [14]), t is the sample thickness, ζ a constant from the samples fixing condition (0.5596 for our case, [15]).

3. Results and discussions

In the next paragraphs we have denoted as a representative sample, the sample for which the obtained mechanical properties values are the closest to the arithmetic mean value of the determined mechanical characteristic, for the whole set of samples of that type.

3.1. Tensile test

In the Figure 4 we present the Hooke graphic for a representative sample which is tensile tested. All the experimental results are written in Table 1.

Table 1. Tensile tests results

	Characteristics			
Corn cob powder + epoxy resin	Modulus of elasticity (MPa) Breaking strength (MPa) Elor		Elongation at break (%)	
Value	193 ± 42	6 ±1	1.6 ± 0.2	

From the Table 1 we can see that our proposed material has low tensile mechanical properties. In [8] there were obtained also low tensile mechanical properties for similar materials, but higher than the ones studied in this research.



Figure 4. The Hooke graphic for a representative sample, tensile tested



3.2. Compression test

In the Figure 5 we present the Hooke graphic for a representative sample tested for compression, with the ratio between the reinforcement and matrix being 50-50. The compression test results are written in Table 2.

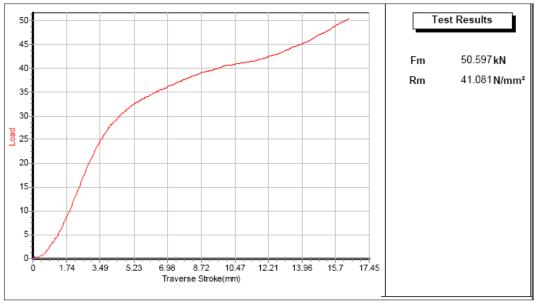


Figure 5. The Hooke graphic for a representative sample with 50-50 ratio between reinforcement and matrix, tested for compression

Table 2. Compression tests results

Corn cob powder + epoxy resin	Characteristic			
	Breaking strength (MPa)	Maximum force (kN)		
50-50	41±3	50.6±7.4		
65-35	25±2.5	25±7.1		
75-25	3+0.5	3.75+0.24		

From the experimental data we can see that our proposed composite has increased mechanical properties at compression compared to the tensile test. We have also obtained increased mechanical properties compared to similar samples (with the same reinforcement but another matrix) like the ones studied in [6].

3.3. Vibrations tests

In the Figure 6 we present the vibration recording (eigenfrequency and damping factor per unit mass determination) in the 65-35 (ratio between reinforcement and matrix) sample, for 140 mm free length. By inserting the experimental values (for the eigenfrequency and damping factor) in (2), (3), (4) and (5) we have determined the other dynamic mechanical characteristics, like: damping factor related to unit mass and length, loss factor, dynamic modulus of elasticity and dynamic rigidity. All the geometrical parameters and the arithmetic mean values for the dynamic mechanical parameters are written in table 3.



Table 3. Free vibrations results (arithmetic mean values) and geometrical characteristics of samples

	Characteristic						
Corn cob powder + epoxy resin	Free length	Damping factor related to unit mass	Eigenfrequency	Density	Specific mass	Dynamic Young modulus	Dynamic stiffness
	100	40.21	141.9	375	0.075	607	0.482
	120	25.49	98.45	375	0.075	606	0.481
	140	20.83	72.72	375	0.075	613	0.487
	160	17.37	55.42	375	0.075	607	0.482
	180	14.56	43.19	375	0.075	590	0.469
Arithmetic mean						604.6	0.4802
	Loss factor	Damping factor related to unit length					
	0.09	6.03					
	0.082	3.82					
	0.091	3.12					
	0.1	2.60					
	0.107	2.18					

In the Table 3, we have expressed the free length in mm, the damping factor related to unit mass in Ns/m/kg, the eigenfrequency in 1/s, the density in kg/m³, the specific mass in kg/m, the dynamic modulus of elasticity in MPa, the dynamic rigidity in Nm² and the damping factor related to unit length in Ns/m/m.

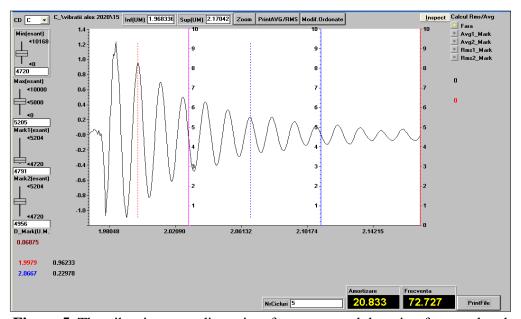


Figure 5. The vibration recording, eigenfrequency and damping factor related to unit mass determination (for the 140 mm free length of the sample)

4. Conclusions

From the experimental results, we can see that our proposed composite has different behaviour at compression compared to the tensile test, with increased mechanical properties at compression. Compared to similar composites from the previous studies, we have obtained increased mechanical properties at compression, but lower for the tensile test.

From the Table 3 where are presented the damping factor values, we can extract the next conclusions:

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these factors must be investigated for each type of bar and material and there could not be obtained a quantitative connection between the factors that affect directly or indirectly the damping phenomenon. The damping is affected by some factors, like: the bars width, thickness or free length, the specific mass, the material amount from a manufactured bar, the elastic and damping characteristics of composing materials. The bars width can affect the damping factor because it establishes the area where the air friction works on the bars.

If we make a comparison between the moduli of elasticity (static and dynamic one), we can see that the dynamic one is 3.13 times higher and the difference between their values is 68%. This result is normal for composite materials because these are an-isotropic and non-homogenous. The result can be explained by the fact that the deformation from the bars free vibrations is very small because the atoms are barely moved from the equilibrium states and a small deformation leads to a high modulus of elasticity. The bars deformation in tensile test is at macro scale, so a high deformation implies a small modulus of elasticity. Also, the first derivative of the applied force with respect to atomic displacement decreases with the separation of the atoms from their mesh network. So, the atoms have an increased displacement in the tensile test which leads to the conclusion that the static modulus of elasticity must be smaller compared to the dynamic one. A similar conclusion was also obtained in the research from [16].

For their obtained mechanical properties, the composites with corn cob powder as reinforcement and epoxy resin as matrix may be used for: making almost-environment-friendly house decorations, table tops, furniture decorations or parts, replacing marble, window sills and so on.

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Manuscript received: 01.11.2021